

Simulation of Acid Gas Removal Unit using MDEA Amine Solvent

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Abstract: The Acid Gas cleaning process used in gas processing plants deploys gas sweetening process. Due to the inexpensive cost of amine solvent, more than 95 % of Gas processing plants use an acid gas removal unit that utilizes an aqueous amine solvent to remove sour gas components such as carbon dioxide (CO₂) and hydrogen sulfide (H₂S). The gas needs to be treated for safety considerations and environmental regulations for H₂S toxicity (H₂S present in sales gas). The heating value of sales gas and CO₂ content needs to be reduced. The acid gas dissolved in water to form acids which causes corrosion, and the equipment needs to be protected. The acid gas needs to be treated to meet the the environmental regulations to reduce SO₂ emissions also called acid rain. The present investigation addresses the performance of using MDEA to determine the absorption capacity of CO₂ & H₂S using Aspen HYSYS software

Keywords: Aspen Hysys V12, Amine, Acid Gas (CO₂& H₂S) Removal, Absorption

INTRODUCTION

Acid gas removal involves the removal of carbon dioxide (CO₂) and/or hydrogen sulfide (H₂S) from vapor streams. Vapor streams containing acid gases enter and are put in contact with a lean solvent in an absorber column. The lean solvent absorbs the acid gases and exits the bottom of the column as a rich solution, which is then sent to a regenerator column to strip the acid gases from the solvent so it can be recycled. Many industries, including oil refining, ammonia plants, natural gas plants, LNG, and hydrogen plants require these processes. For property packages three acid gas cleaning packages are available. Acid gas chemical solvents

The acid gas chemical solvents package is used to simulate typical acid gas removal through absorption into amine solvents. It uses Electrolyte nonrandom two liquid model for thermodynamics. It used Peng Robinson equation of state for vapor phase properties.

- Acid gas physical solvents

The acid gas physical solvents property package is designed to use in systems for removal using dimethyl ether of polyethylene glycol (DEPG). Physical solvents have low solvent regeneration requirements but higher association with hydrocarbons. Physical solvents are favorable for bulk removal of acid gases at high pressure. The Perturbed Chain - Statistical Associating Fluid Theory (PC SAFT) Equation of state is used to model the interactions of DEPG with other components.

- Acid gas liquid treating.

The acid gas liquid treating is designed for bulk removal of acid gases at high pressures. Liquid treating occurs at low temperatures and high pressure. A liquid liquid extractor is used instead of an absorber column. The property package used Electrolyte Non-Random Two Liquid (ENRTL) model for thermodynamics. It uses Peng Robinson equation of state for vapor phase properties. Selection of acid gas property package will automatically add selection of reactions to Aspen hysys model. These reactions are made to emulate chemistry that occurs between amines, water and acid gas. Reaction set 1 covers reaction in Absorber, Reaction set 2 covers reaction in Regenerator. Reaction set 3 is used for reaction equilibria. The kinetic reaction model is represented by

$$K = A * e^{(-E/RT)} * T^B$$

Where, A- frequency factor

E- Activation Energy, B- Extended rate reaction constant

On an industrial scale, chemical solvents are used for the separation of CO₂ which is based on the amine scrubbing technique. The aqueous solution of the amine-based scrubbing technique is a highly mature and mostly practiced technique in the CO₂ capture process on an industrial scale. Amines are further divided into three different categories; primary, secondary, and tertiary amines, depending upon their one, two, or three hydrogen atoms which are replaced by the alkyl functional group. Monoethanolamine (MEA), diethanolamine (DEA), N-methyl diethanolamine (MDEA), diglycolamine (DGA), diisopropanolamine (DIPA), 2-amino-2-methyl-1-propanol (AMP), and piperazine (PZ) are some of the most commonly utilized aqueous alkanolamines in the absorption process.

Even though alkanolamines have numerous applications industrially, and are frequently used solvent, still have many demerits, which includes low loading of CO₂, high loss of vapors, corrosion of equipment, and consumption of high energy, thermal and oxidative degradation. According to the stoichiometric analysis, the loading capacity of primary and secondary amines (MEA and DEA) is restricted to 0.5 moles of CO₂ per mole of amine. The tertiary amines MDEA and TEA have recently become very important amines because it is selective and more ideal for H₂S but having the high capacity to remove CO₂, loss of low vapors, enthalpy of reaction with CO₂ is very low, high thermal stability, low vapors loss, and low enthalpy of reaction with CO₂, the most vital property in the regeneration of amines.

This study aims to investigate the capture of both CO₂ and H₂S using a novel amine blend to find out the solubility of CO₂ and H₂S. MDEA is selected as the main amine in this study. The concentration of H₂S and CO₂ in sweet gas using MDEA at 25 °C to 50 °C and at pressure of 57 bar was investigated by using the Aspen HYSYS V12 simulator.

METHODOLOGY

The present work was completed by using Aspen HYSYS V12.1, a commonly used software for acid gas removal unit (AGRU) in different oil and gas fields. The Acid Gas (chemical solvent) built-in thermodynamic package was used for this simulation because both solvents are chemical solvents, and the Acid Gas package produces output with lesser deviation.

The Acid Gas – Chemical Solvents package in Acid Gas technology supports solvents including MDEA, DEA, MEA, DGA, DIPA, PZ and TEA. It also supports solvent blends including Sulfolane + DIPA, Sulfolane + MDEA, Sulfolane + MDEA + PZ, MDEA+ MEA + DEA and any two chemical solvents. The Acid Gas - Chemical Solvents package is developed with the Peng-Robinson equation of state for vapor phase and electrolyte NRTL (eNRTL) for electrolyte thermodynamics.

PROCESS DESCRIPTION

A feed stream of natural gas with bulk spec concentration of CO₂ and H₂S containing above specification levels of acid gases (both CO₂ and H₂S) and Lean amine solution of 45wt% MDEA and 55 wt% Water. The absorber is critical unit in acid gas cleaning. It contains 20 trays and operates at high pressure. The sour feed gas and lean amine enters the column while sweet gas and rich amine exits the column. The temperature in the absorber can range from 15-65°C.

Higher temperature helps prevent condensation and foaming. Other factors that affect performance can include strength of amine, flowrate and impurity loading in amine.

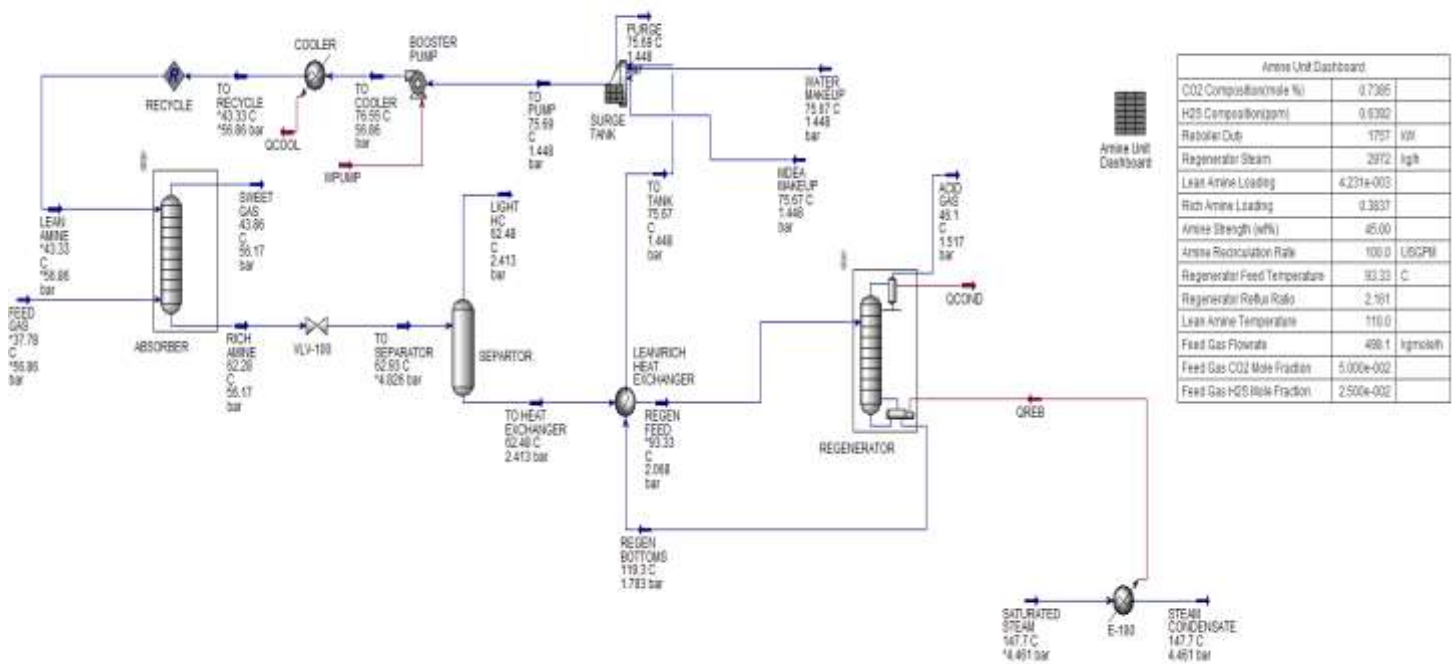
Most of the mass transport occurs in bottom half of the column. A phenomenon called ‘temperature bulge’ can occur due to high heat of absorption generated by mass transfer. Heat is quickly carried by the column by liquid flow so heat travels upwards with the vapor flow. Increase in vapor flow rate will increase temperature bulge.

The separator flashes rich amine to low pressure. It is used to separate dissolved sweet gas. Dissolved hydrocarbons can cause foaming Residence time can be over 20 minutes. Light hydrocarbon liquids are skimmed within the flash tank.

Regenerator allows for reclamation of amine by separation. It is energy intensive process. The heat exchanger preheats the regenerator feed stream with bottoms product stream from absorber. This heat integration controls the temperature profiles in the system and reduces the amount of cooling and heating energy that needs to be used in the process. Passing as much heat as possible from the lean amine to rich amine provides the most favorable heat integration. The regenerator heats the amine solution unbinding the contaminants from amine solution. This takes place at elevated temperatures and low pressures to facilitate the separation. The condenser will not condense CO₂ and H₂S instead only returning water, amine and hydrocarbons. Common reflux ratio range from 1 to 3. The reboilers are major cost center to the Column. A typical Reboiler duty is 6 MMBtu/hr. The lean amine solution from the column leaves through bottom of column and sent to lean/rich heat exchanger.

The Concentrated contaminants stream leaves through top of column for further process. To keep the process at steady state a storage tank is used to provide makeup water and lean amine. This restores the amine solution to its original strength. Replenishing losses due to separation operation or formation of heat stable salts. In addition, a portion of lean amine called the slip stream is diverted to remove contaminants such as iron sulfides. Subsequent pumping and cooling will bring the recycled amine for conditions to required to be used in absorber. This closes the recycle loop for lean amine. Process limits for the sweet gas stream is 4 ppmv H₂S and 2% CO₂ by volume.

Process Simulation of Acid Gas Cleaning Using MDEA



SIMULATION BASIS

The default method for acid gas cleaning is efficiency mode. The calculations in Aspen Hysys assumes the two film Theory assumes the resistance to heat and mass transfer is concentrated in two films one for each phase. In efficiency mode this theory is used to determine mass fluxes and efficiencies for CO₂ and H₂S only. The model does not account for resistance to heat transfer or further discretized the films. It accounts conversion for CO₂, H₂S and amines in fluxes while the other compounds are determined with equilibrium calculations and efficiencies. It is possible to specify efficiencies for these other components. It relies on equilibrium model for material/energy balances. Acid gas in Aspen Hysys is rate-based technology.

Acid Gas in Aspen HYSYS accounts for not only kinetic reaction rate-based modeling, but it also accounts for mass transfer resistance. The Acid Gas technology provides Efficiency Modeling mode and Advanced Modeling mode for

different levels of model fidelity. Advanced Modeling mode can be used to identify bulge-pinch and lean-pinch absorber columns. One can plot absorber temperature by stage in Aspen HYSYS and see the corresponding efficacy of the absorption.

One can just plot the partial pressure of H₂S or CO₂ by stage in the vapor vs. aqueous phases to see if the column is pinched. Efficiency mode accounts for mass-transfer resistance at the vapor-liquid interface to calculate “rate-based” efficiencies for H₂S and CO₂, and this mode allows the HYSIM I/O algorithm to be used in the column. The Advanced Modeling mode accounts for mass-transfer resistance at the vapor-liquid interface to calculate the flux of all components, and this mode uses the rate-based distillation directly.

PROCESS SIMULATION

This study consists of a liquid-liquid acid gas treating process using MDEA as a chemical solvent at high pressure to remove H₂S and CO₂ from acid feed gas. 9610 kg/hr of acid gas feed (2.5 mol% H₂S and 5 mol% CO₂) is fed to Absorber (57 bar), where the H₂S is removed to < 10 ppm H₂S in the overhead hydrocarbon product (mostly C₃). Acid gases are stripped from amine by a regenerator column at low pressure (1.5 bar) and high temperature (119 °C) from the MDEA solvent, which is recycled with makeup back to the extractor column. The Feed Gas enters the absorber at 56.86 bar and temperature 38 °C where acid gases are absorbed with lean amine and the sweet gas (sales gas) from the top of absorber is achieved with desired spec. The bottom rich amine from absorber at temperature of 63 °C is fed to separator where light hydrocarbons are flashed and the outlet is preheated with the bottoms from regenerator at temperature of 93 °C fed to Regenerator. In Regenerator the rich amine is stripped of acid gases (H₂S and CO₂) at a reboiling temperature of 147 °C and heat duty of 1757 KW. The stripped rich amine from bottom of Regenerator at temperature of 119 °C is cooled to 76 °C in lean/rich heat exchanger and fed to surge tank for makeup lean amine going to absorber. The desired sales gas specification of less than 10 ppm H₂S gas and 0.74 mol% (<2 mol%) CO₂ in sweet gas is achieved with MDEA as amine solvent.

Input specification for Aspen Hysys Simulation

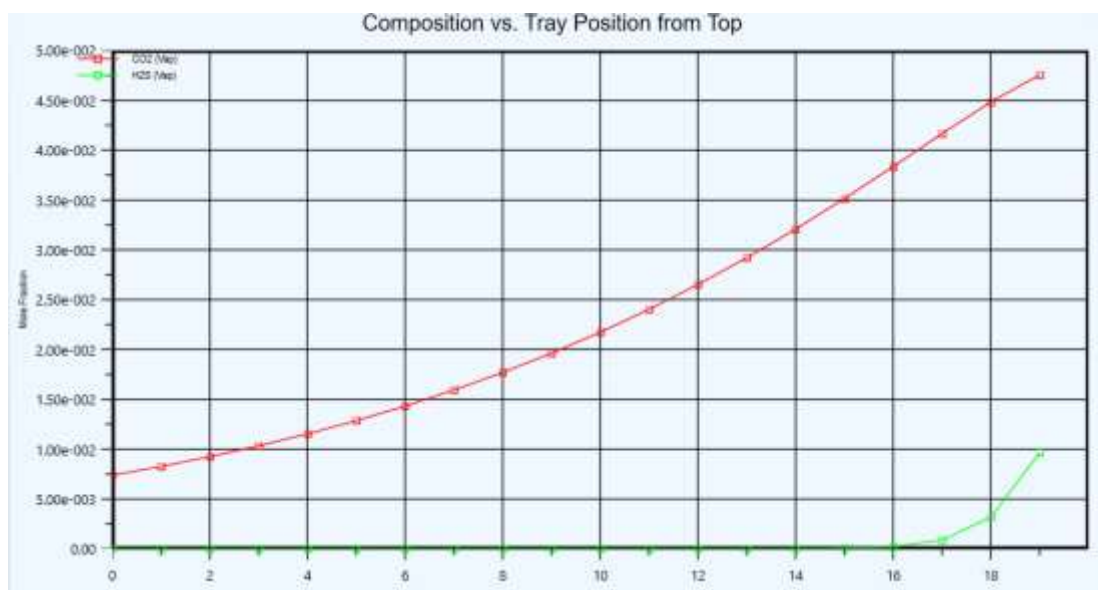
Parameters	
Gas flowrate (kgmole/hr)	498.1
Gas temperature (°C)	38
Gas pressure (bar)	57
Composition of CO ₂ in feed gas (mole fraction)	0.05
Composition of H ₂ S in feed gas (mole fraction)	0.025
Solvent flowrate (m ³ /h)	24
Solvent temperature °C	43
solvent pressure (bar)	57

Absorber trays	20
Regenerator trays	10
Condenser temperature °C	46
Reboiler temperature °C	148

RESULT AND DISCUSSION

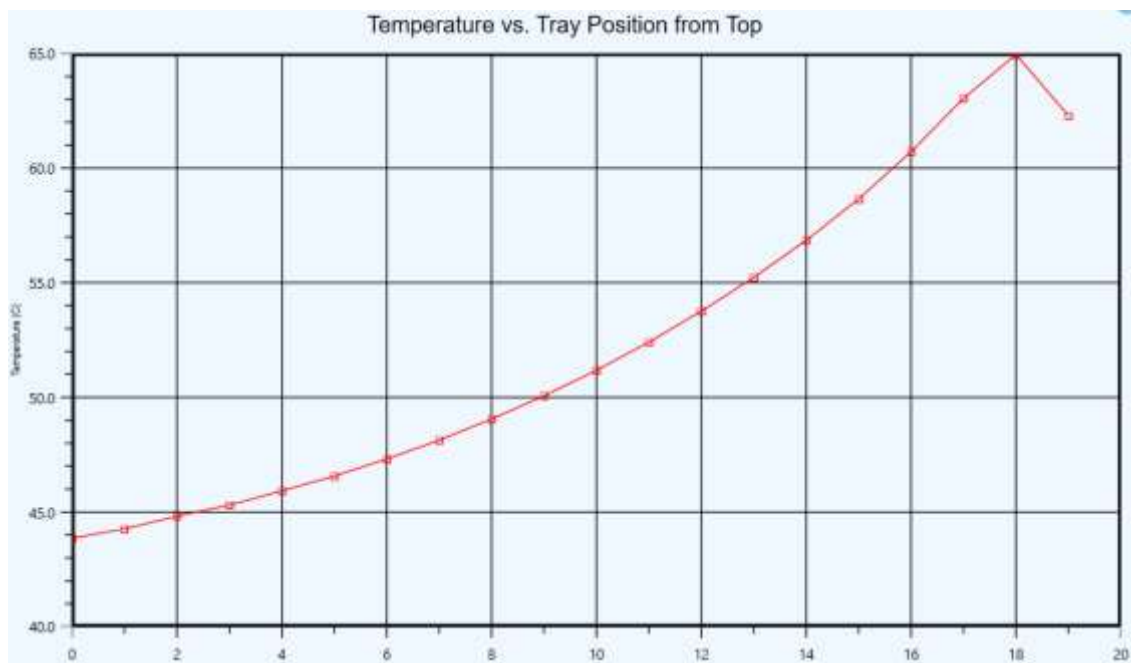
- Effect of Composition vs Tray Position from Top**

It can be seen from the composition vs the tray position from top curve that as the acid gas rises in the absorber with countercurrent flow of lean MDEA Solution, the H₂S concentration gradually decrease from 2.5 mole % at 20th tray to zero mole % at first tray. Similarly, the CO₂ concentration gradually decrease from 5 mole % at 20th tray to less than 1 mole %. at first tray. This shows that the most of mass transfer from acid gas to lean MDEA solution takes place at the bottom of the Absorber.



- Effect of Temperature vs Tray Position from Top**

Also, it can be seen that as the acid gas rises to top in the Absorber, Temperature bulge occurs in the column with temperature rising highest at tray eighteen in the bottom of the absorber. This temperature rise is due to high heat of absorption taking place at the maximum mass transfer towards the bottom of the absorber.



CONCLUSION

The overall CO₂ and H₂S absorption in a MDEA solution was investigated using Aspen HYSYS simulation software. It is investigated that the tertiary amines MDEA have recently become very important amines because it is selective and more ideal for H₂S and having the high capacity to remove CO₂ using the Acid Gas Cleaning -Chemical Solvent Property Package in Aspen Hysys V12. The effect of composition and Temperature on tray position from top was studied and it is observed that the bulk of mass transfer takes place at the bottom of the Absorber with high temperature in the Rich Amine outlet in the Absorber due to high heat of Absorption.

REFERENCES

1. Lunsford KM, Bullin JA. 2006 Optimization of Amine Sweetening Units Ind Eng Chem Res 43 987-991.
2. Abkhiz V, Heydari I. 2014 Comparison of amine solutions performance for gas sweetening. Asia- Pacific J Chem Eng 9 656-662.
3. Kidnay AJ, Kidnay AJ, Parrish WR. 2006 Fundamentals of Natural Gas Processing. Fundam Nat Gas Process 27 65-71.
4. Lim W, Choi K, Moon I. 2013 Current Status and Perspectives of Liquefied Natural Gas Plant Design. Ind Eng Chem Res 52 3065-3088.
5. Al-Lagtah NMA, Al-Habsi S, Onaizi SA. 2015 Optimization and performance of Lekhwair natural gas sweetening plant using Aspen HYSYS. J Nat Gas Sci Eng 26 367-381.
6. Zahid, U.; Al Rowaili, F.N.; Ayodeji, M.K.; Ahmed, U. Simulation and parametric analysis of CO₂ capture from natural gas using diglycolamine. Int. J. Greenh. Gas Control 2017, 57, 42–51.
7. Bonenfant, D.; Mimeault, M.; Hausler, R. Estimation of the CO₂ Absorption Capacities in Aqueous 2-(2-Aminoethylamino) ethanol and Its Blends with MDEA and TEA in the Presence of SO₂. Ind. Eng. Chem. Res. 2007, 46, 8968–8971.
8. Ban, Z.H.; Keong, L.K.; Shariff, A.M. Physical Absorption of CO₂ Capture: A Review. Adv. Mater. Res. 2014, 917, 134–143
9. Mudhasakul, S.; Ku, H.-M.; Douglas, P.L. A simulation model of a CO₂ absorption process with methyl diethanolamine solvent and piperazine as an activator. Int. J. Greenh. Gas Control 2013, 15, 134–141.
10. Thitakamol, B.; Veawab, A. Foaming model for CO₂ absorption process using aqueous monoethanolamine solutions. Colloids Surfaces A Physicochem. Eng. Asp. 2009, 349, 125–136.
11. Sarker, N.K. Theoretical effect of concentration, circulation rate, stages, pressure and temperature of single amine and amine mixture solvents on gas sweetening performance. Egypt. J. Pet. 2016, 25, 343–354
12. Banat, F.; Younas, O.; Didarul, I. Energy and exergetic dissection of a natural gas sweetening plant using methyldiethanol amine (MDEA) solution. J. Nat. Gas Sci. Eng. 2014, 16, 1–7.

13. Lunsford, K.M.; Bullin, J.A. Optimization of Amine Sweetening Units; Bryan Research and Engineering, Inc.: Bryan, TX, USA, 2006
14. Zahid, U. Simulation of an Acid Gas Removal Unit Using a DGA and MDEA Blend Instead of a Single Amine. Chem. Prod. Process Model. 2020, 15.
15. Maceiras, R.; Álvarez, E.; Cancela, M.Á. Effect of temperature on carbon dioxide absorption in monoethanolamine solutions. Chem. Eng. J. 2008, 138, 295–300.
16. Simulation of Natural Gas Treatment for Acid Gas Removal Using the Ternary Blend of MDEA, AEEA, and NMP, Sustainability, MDPI, Aug 2022
17. Simulation of acid gas removal unit using DIPA+TEA amine solvent, IOP Conference Series: Materials Science and Engineering, 2022