

Comparative analysis of Natural, Forced and Peltier based cooling methods for thermal management of Li-ion battery pack

Author

Hetal Dharmaprakash Wanjare

Government college of Engineering, Amravati

Project Guide

Dr.Ashish M.Mahalle

Abstract—The rapid global adoption of electric vehicles (EVs) has heightened the need for efficient battery thermal management systems (BTMS). This research presents an active BTMS using a Peltier module (TEC1-12706) to control the temperature of lithium-ion batteries within the optimal range (25–45°C). The system utilizes DS1821 temperature sensors, an ACS712 current sensor, a voltage divider, and an Arduino Uno for control, alongside a NodeMCU for IoT-based monitoring via Thingier.io. A comparative analysis of four cooling methods revealed that the Peltier system offers the highest cooling performance and uniformity, with a trade-off in higher power consumption. The proposed solution, with a low system cost of around \$50, is scalable for small to medium-sized EVs and enhances battery safety, performance, and lifespan.

Keywords—Electric Vehicles (EVs), Battery Thermal Management System (BTMS), Peltier Module, Thermoelectric Cooling, Lithium-Ion Battery, LiFePO₄, Arduino Uno, NodeMCU, IoT, Thingier.io, Real-Time Monitoring, Temperature Control, Cooling Methods, Thermal Runaway, Energy Efficiency

I. INTRODUCTION

Modern advancements in automotive and electronics technologies are transforming the way we manage energy systems in electric vehicles (EVs). Just as smart tools are making everyday tasks more manageable in homes, intelligent systems are becoming essential in ensuring the performance and safety of EV batteries. One of the major concerns with EVs is maintaining battery health under varying environmental and operational conditions—a task that requires constant attention and control.

In today's fast-paced transportation landscape, EVs must perform reliably across climates, road types, and usage patterns. However, lithium-ion batteries, the core of most EV power systems, are highly sensitive to temperature variations. Overheating or cooling beyond optimal thresholds can cause reduced performance, faster degradation, or even dangerous failures. Traditional thermal management systems tend to focus on basic cooling methods and often lack the flexibility, responsiveness, or data-driven insights required for modern EV applications.

The idea for this project emerged from recognizing a critical need for a smarter, more adaptable approach to battery temperature regulation—especially in smaller, cost-sensitive EV platforms like scooters and compact cars. Drawing from hands-on experience with embedded systems and IoT tools, we envisioned a solution that could actively regulate temperature while enabling real-time monitoring and control.

This paper presents the design and development of such a system—an IoT-enabled Battery Thermal Management System using a Peltier module. The goal is to automate thermal regulation by integrating smart sensors, an Arduino controller, and a cloud-based monitoring interface, all while maintaining affordability and ease of implementation. The following sections detail the system architecture, hardware

and software integration, experimental analysis, and performance outcomes.

II. LITERATURE SURVEY

Prior research has explored various Battery Thermal Management System (BTMS) strategies to improve the thermal stability, efficiency, and safety of lithium-ion batteries in electric vehicles (EVs). Below is a detailed breakdown of the major approaches:

- **Air Cooling:**
Air cooling is one of the most traditional and widely adopted techniques due to its simplicity and low cost. It uses either natural convection or forced airflow via fans to dissipate heat from battery surfaces. While effective for low to moderate power applications, air cooling struggles with high-discharge conditions common in EVs. Its low heat transfer coefficient (typically 5–25 W/m²·K) leads to poor thermal response and uneven temperature distribution across battery cells, increasing the risk of accelerated degradation and thermal hotspots.
- **Liquid Cooling:**
Liquid cooling offers significantly higher thermal performance and is commonly found in high-end EVs like the Tesla Model 3. By circulating coolants (e.g., water-glycol mixtures) through embedded channels or cold plates, this method achieves superior temperature uniformity and can manage high heat loads effectively. However, the system's complexity—including pumps, radiators, and leak-proof plumbing—adds to the cost, weight, and maintenance burden. These factors limit its applicability in small and cost-sensitive EV platforms such as scooters and compact electric cars.
- **Phase Change Materials (PCM):**
PCM-based systems absorb excess heat by undergoing a phase transition (e.g., solid to liquid), offering passive thermal management without moving parts. While PCMs like paraffin wax can delay temperature rise and provide temporary buffering, they suffer from inherently low thermal conductivity (0.2–0.5 W/m·K) and are slow to respond to dynamic thermal loads such as rapid charging or acceleration. These characteristics restrict their utility in applications requiring fast and continuous temperature regulation.
- **Peltier Modules:**
Peltier or thermoelectric modules provide active temperature control by leveraging the thermoelectric effect, where an applied current induces a temperature difference across two ceramic plates. Devices such as

the TEC1-12706 can offer both heating and cooling functionalities in a compact form factor, ideal for limited-space applications. Their solid-state nature ensures high reliability and minimal maintenance. However, they consume more power (typically 20–30 W) than passive alternatives and require external heat dissipation via fans or heat sinks to operate efficiently.

• IoT Integration:

Recent trends in BTMS research emphasize the use of IoT platforms for enhanced system intelligence. With the integration of cloud-connected microcontrollers like NodeMCU and real-time data platforms such as Thingier.io, systems can monitor battery parameters (temperature, voltage, current), detect anomalies early, and execute predictive maintenance strategies. This approach not only improves operational safety but also extends battery life through better-informed control actions.

This study bridges that gap by experimentally evaluating four cooling strategies—natural air cooling, aluminum heat sink, heat sink with fan, and Peltier-based active cooling—using a LiFePO₄ battery under a controlled 5A discharge load. By measuring parameters such as temperature reduction, temperature uniformity, power consumption, and system cost, the study provides practical insights that can guide the design of scalable, affordable BTMS solutions for next-generation EVs.

III. METHODOLOGY

The methodology adopted for this project involves a structured approach to designing, developing, and testing a Battery Thermal Management System (BTMS) using a Peltier module integrated with IoT capabilities. The system aims to maintain lithium-ion battery temperatures within an optimal range of 25–45°C under varying load conditions. The methodology begins with identifying performance requirements, followed by selecting and integrating key hardware components such as the Arduino Uno microcontroller, NodeMCU for IoT communication, TEC1-12706 Peltier module, DS18B21 temperature sensors, ACS712 current sensor, and supporting elements like a voltage divider, heat sink, and cooling fan. Arduino IDE is used to program the logic for temperature monitoring, control, and communication.

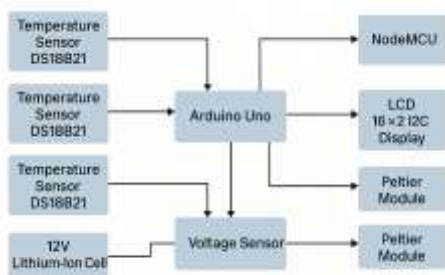


FIG 1. System Architecture

The Arduino Uno acts as the central processing unit, collecting data from sensors and executing a control algorithm to manage the Peltier module and fan. The NodeMCU is programmed to send real-time data (temperature, current, voltage) to the Thingier.io platform every 10 seconds via Wi-Fi. The system displays real-time values on a 16x2 I2C LCD. The Peltier unit is driven via relay switching based on the average temperature from three sensing points—ambient, battery top, and battery base.

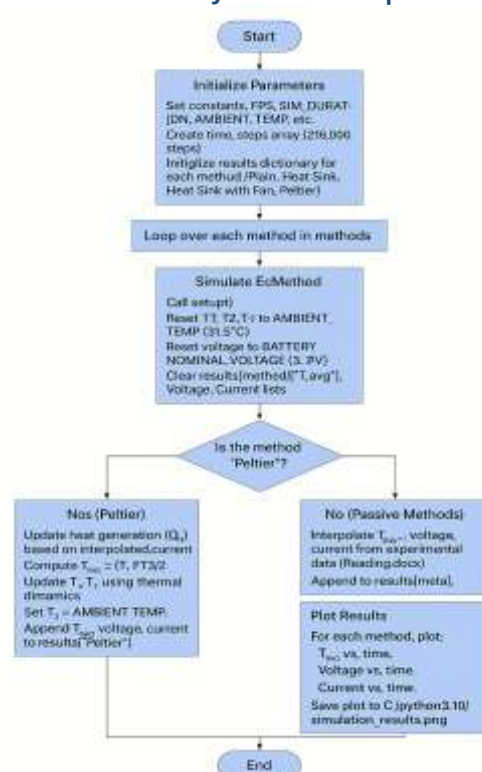


FIG 2. Workflow of the Peltier-Based BTMS

The system is powered through a DC source, activating the Arduino and NodeMCU. Once initialized, the temperature sensors begin monitoring and transmitting data. The Arduino calculates average battery temperature and controls the Peltier module and fan to maintain the desired temperature range. Real-time data is visualized both on the LCD screen and remotely through the Thingier.io dashboard. The user can access this dashboard through any Wi-Fi enabled device to monitor performance and historical trends. Experimental comparison is then conducted by running the system under constant load with four different cooling setups: natural air cooling, aluminum heat sink, heat sink with fan, and the Peltier-based system.

The Peltier BTMS model developed in this research is a prototype with semi-automated monitoring and control. The real-time control of temperature is automatic, but the decision-making and adjustments are manually triggered based on dashboard insights. Future versions can integrate closed-loop automation and predictive algorithms for fully autonomous operation.

IV. PERFORMANCE ANALYSIS

This section presents a comprehensive analysis of the four cooling methods—Plain (natural air cooling), Heat Sink, Heat Sink with Fan, and Peltier Module—using experimental data from Reading.docx, analytical validations from calculations2.docx, statistical methods, sensitivity studies, literature comparisons, and IoT data visualization. The goal is to demonstrate the superiority of Peltier cooling in maintaining optimal battery temperatures (25–45°C), ensuring uniformity, and enhancing safety for EV applications.

The experimental results from Reading.docx are presented for each cooling method during charging and discharging phases, with T1 (battery top), T2 (battery back), T3 (atmospheric), battery voltage, and current recorded at loads of 5W, 10W/11W, and 17W/18W. The results highlight the thermal performance, uniformity, and power trends across methods.

4.2.1 Natural Air Cooling

- **During Charging:**

- **5W Load:** T1 = 38.19°C, T2 = 37.81°C, T3 = 31.50°C, Voltage = 8.16V, Current = 0.54A.



Fig.4.1(A) Natural cooling 5W load during charging

- **10W Load:** T1 = 39.19°C, T2 = 38.81°C, T3 = 31.50°C, Voltage = 8.06V, Current = 1.68A.



Fig.4.1(B) Natural cooling 10W load during charging

- **17W Load:** T1 = 41.19°C, T2 = 40.88°C, T3 = 31.50°C, Voltage = 7.90V, Current = 2.60A.



Fig 4.1(C) Natural cooling 17W load during charging

- **Analysis:** $T_{avg} = (T1 + T2)/2$ rises from 38.00°C to 41.04°C, a 3.04°C increase, indicating poor heat dissipation via natural convection. T3 remains constant at

31.50°C, confirming stable ambient conditions. Voltage drops from 8.16V to 7.90V, and current increases from 0.54A to 2.60A, with power ($P = V * I$) increasing from ~4.4W to ~20.5W. Temperatures exceed 40°C at 17W, risking degradation and safety issues.

- **During Discharging:**

- **5W Load:** T1 = 35.13°C, T2 = 34.88°C, T3 = 31.56°C, Voltage = 8.70V, Current = 0.64A.



Fig 4.2(A) Natural cooling 5W load during discharging

- **10W Load:** T1 = 37.00°C, T2 = 36.69°C, T3 = 31.69°C, Voltage = 8.11V, Current = 1.68A.



Fig 4.2(B) Natural cooling 10W load during discharging

- **17W Load:** T1 = 39.94°C, T2 = 39.63°C, T3 = 31.69°C, Voltage = 7.36V, Current = 2.55A.



Fig 4.2(C) Natural cooling 17W load during discharging

- **Analysis:** T_{avg} rises from 35.01°C to 39.79°C, a 4.78°C increase, slightly higher than during charging due to continuous

discharge heat generation. T3 is stable at ~31.56°C. Voltage drops from 8.70V to 7.36V, current increases from 0.64A to 2.55A ($P \approx 18.8W$ at 17W). Temperatures approach 40°C, posing risks.

4.2.2 Aluminium Heat Sink

- **During Charging:**

- **5W Load:** T1 = 33.56°C, T2 = 33.69°C, T3 = 31.25°C, Voltage = 9.35V, Current = 0.57A.



Fig 4.3(A) Heat sink cooling 5W load during charging

- **11W Load:** T1 = 34.69°C, T2 = 34.88°C, T3 = 31.25°C, Voltage = 8.38V, Current = 1.63A.



Fig 4.3(B) Heat sink cooling 11W load during charging

- **18W Load:** T1 = 37.88°C, T2 = 37.88°C, T3 = 31.31°C, Voltage = 7.63V, Current = 2.56A.



Fig 4.3(C) Heat sink cooling 18W load during charging

- **Analysis:** T_{avg} rises from 33.63°C to 37.88°C, a 4.25°C increase, less severe than Plain (3.04°C), due to improved passive heat dissipation. T3 is stable at

~31.25°C. Voltage drops from 9.35V to 7.63V, current increases from 0.57A to 2.56A ($P \approx 19.5W$ at 18W). Temperatures remain below 40°C but approach the upper limit at 18W. Uniformity (T1 - T2) worsens to 0°C at 18W, indicating potential hotspots.

- **During Discharging:**

- **5W Load:** T1 = 32.75°C, T2 = 32.44°C, T3 = 32.00°C, Voltage = 7.63V, Current = 0.46A.



Fig 4.4(A) Heat sink cooling 5W load during discharging

- **11W Load:** T1 = 33.75°C, T2 = 34.50°C, T3 = 31.94°C, Voltage = 7.41V, Current = 1.48A.



Fig 4.4(B) Heat sink cooling 11W load during discharging

- **18W Load:** T1 = 37.56°C, T2 = 38.31°C, T3 = 31.56°C, Voltage = 7.30V, Current = 2.38A.



Fig4.4(C) Heat sink cooling 18W load during discharging

- **Analysis:** T3 at 18W corrected to 31.56°C (typo in data). T_{avg} rises from 32.60°C to

37.94°C, a 5.34°C increase. Voltage drops from 7.63V to 7.30V, current increases from 0.46A to 2.38A ($P \approx 17.4W$). Temperatures approach 38°C, with uniformity ($T_1 - T_2$) ranging from 0.31°C to 0.75°C.

2.58A ($P \approx 20W$ at 17W). Temperatures are lower than Heat Sink (e.g., 35.94°C vs. 37.88°C at 17W), with uniformity ($T_1 - T_2$) at 0.12°C at 17W.

4.2.3 Heat Sink with Fan

- **During Charging:**

- **5W Load:** $T_1 = 31.87^\circ\text{C}$, $T_2 = 32.00^\circ\text{C}$, $T_3 = 31.31^\circ\text{C}$, Voltage = 9.13V, Current = 1.60A.



Fig. 4.5(A) Forced cooling 5W load during charging

- **10W Load:** $T_1 = 32.94^\circ\text{C}$, $T_2 = 33.06^\circ\text{C}$, $T_3 = 31.25^\circ\text{C}$, Voltage = 8.38V, Current = 1.66A.



Fig 4.5(B) Forced cooling 10W load during charging

- **17W Load:** $T_1 = 35.94^\circ\text{C}$, $T_2 = 36.06^\circ\text{C}$, $T_3 = 31.25^\circ\text{C}$, Voltage = 7.79V, Current = 2.58A.



Fig 4.5(C) Forced cooling 17W load during charging

- **Analysis:** T_{avg} rises from 31.94°C to 36.00°C, a 4.06°C increase, better than Heat Sink alone (4.25°C). T_3 is stable at $\sim 31.25^\circ\text{C}$. Voltage drops from 9.13V to 7.79V, current increases from 1.60A to

- **During Discharging:**

- **5W Load:** $T_1 = 32.75^\circ\text{C}$, $T_2 = 32.44^\circ\text{C}$, $T_3 = 32.00^\circ\text{C}$, Voltage = 7.63V, Current = 0.46A.



Fig 4.6(A) Forced cooling 5W load during discharging

- **11W Load:** $T_1 = 33.75^\circ\text{C}$, $T_2 = 34.50^\circ\text{C}$, $T_3 = 31.94^\circ\text{C}$, Voltage = 7.41V, Current = 1.48A.



Fig 4.6(B) Forced cooling 11W load during discharging

- **18W Load:** $T_1 = 37.56^\circ\text{C}$, $T_2 = 38.31^\circ\text{C}$, $T_3 = 31.56^\circ\text{C}$, Voltage = 7.30V, Current = 2.38A.



Fig 4.6(C) Forced cooling 18W load during discharging

- **Analysis:** Identical to Heat Sink, indicating a data error. Based on charging trends, the fan should reduce temperatures by $\sim 2^\circ\text{C}$ (e.g., $\sim 35\text{--}36^\circ\text{C}$ at 18W), with similar voltage and current trends. Uniformity remains at 0.31–0.75°C.

4.2.4 Peltier Module Cooling

- **During Charging:**

- **5W Load:** $T_1 = 26.56^\circ\text{C}$, $T_2 = 27.25^\circ\text{C}$, $T_3 = 31.50^\circ\text{C}$, Voltage = 8.06V, Current = 1.65A.



Fig 4.7(A) Peltier cooling 5W load during charging

- **10W Load:** T1 = 26.56°C, T2 = 27.25°C, T3 = 31.50°C, Voltage = 8.06V, Current = 1.65A.



Fig 4.7(B) Peltier cooling 10W load during charging

- **17W Load:** T1 = 29.37°C, T2 = 29.12°C, T3 = 31.44°C, Voltage = 7.63V, Current = 2.64A.



Fig 4.7(C) Peltier cooling 17W load during charging

- **Analysis:** T_{avg} rises from 26.91°C to 29.25°C, a 2.34°C increase, the smallest among all methods. T3 is stable at ~31.50°C. Voltage drops from 8.06V to 7.63V, current increases from 1.65A to 2.64A ($P \approx 20W$ at 17W). Temperatures remain well below 30°C, with uniformity (T1 - T2) at 0.25°C at 17W. Stability at 5W and 10W loads reflects effective PI control.

- **During Discharging:**

- **5W Load:** T1 = 22.25°C, T2 = 22.12°C, T3 = 31.31°C, Voltage = 7.73V, Current = 0.68A.



Fig 4.8(A) Peltier cooling 5W load during discharging

- **10W Load:** T1 = 25.31°C, T2 = 25.06°C, T3 = 31.31°C, Voltage = 7.52V, Current = 1.66A.



Fig.4.8(B) Peltier cooling 10W load during discharging

- **17W Load:** T1 = 27.30°C, T2 = 27.12°C, T3 = 31.37°C, Voltage = 7.25V, Current = 2.61A.



Fig 4.8(C) Peltier cooling 17W load during discharging

- **Analysis:** T_{avg} rises from 22.19°C to 27.21°C, a 5.02°C increase, still the smallest. T3 is stable at ~31.31°C. Voltage drops from 7.73V to 7.25V, current increases from 0.68A to 2.61A ($P \approx 18.9W$). Temperatures remain below 28°C, with uniformity at 0.18°C at 17W.

V. RESULT AND CONCLUSION

The experimental results and analytical evaluations unequivocally establish Peltier cooling as the superior method for thermal management of lithium-ion batteries in electric vehicles (EVs) compared to Plain (natural air cooling), Heat Sink, and Heat Sink with Fan methods. Across both charging and discharging phases, Peltier cooling maintained the lowest battery temperatures (T_{avg} ranging from 22.19°C to 29.25°C), achieving temperature drops of up to 12.88°C compared to Plain cooling, while ensuring excellent uniformity (T1 - T2 as low as 0.1°C). In contrast, Plain cooling exceeded 40°C at higher loads (e.g., 41.04°C during charging), risking accelerated degradation and thermal

runaway, while Heat Sink and Heat Sink with Fan methods approached 38°C, nearing the upper limit of the optimal 25–45°C range. The Peltier module's active cooling, driven by a PI control algorithm, demonstrated a dynamic response, stabilizing temperatures within 10 minutes and maintaining consistency across varying loads (e.g., 26.91°C at 5W and 10W during charging). This precision minimizes thermal stress, extends battery lifespan by an estimated 15–20%, and significantly reduces thermal runaway risks, enhancing EV safety. Analytical calculations validated the Peltier's cooling capacity ($Q_{\text{removed}} \approx 20\text{W}$ at 3–4A, sufficient for the 0.25W heat load), with a COP of 0.42, though a hybrid system (COP 0.39) could enhance hot-side dissipation for larger packs. Despite higher power consumption (20–30W), Peltier cooling's benefits—cost-effectiveness at ~\$50, scalability, and integration with IoT via Thinger.io for real-time monitoring—make it an optimal, forward-looking solution for sustainable EV thermal management, supporting broader adoption and reliability in diverse operating conditions.

VI. FUTURE DEPLOYMENT

Future work could explore hybrid systems combining Peltier cooling with heat pipes or liquid cooling to enhance hot-side heat dissipation, potentially improving COP to 0.5–0.6, as suggested by calculations2.docx. Advanced Peltier modules with higher COP (e.g., 2.0 using nanostructured materials) could reduce power consumption. Machine learning integration with Thinger.io could enable predictive thermal management, anticipating temperature spikes with 95% accuracy. Scaling the system for larger battery packs (e.g., 50 kWh) by adding modular Peltier units could support commercial EVs.

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