Structural Analysis of Foot Step Bearing

To study the various factors that influence life of the bearing in rotating systems.

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Abstract - To study the various factors when the bearing is used to support a shaft which is placed vertically with axial load that influence the life of the bearing. Years of field experience and laboratory testings, together with advanced calculations, form the base for development of computer programs used to analyze and dimension the rotating system where bearing and shaft plays an important role.

Keywords - Bearing Design Parameters, Load Factors, Equations, Structural Analysis Results.

I. INTRODUCTION

Bearings are one of the key components that determine the service interval for rotating machinery; they can even limit the life of the machine. Therefore, knowledge and understanding of bearings are important to both designers and users. In selecting the bearing to be used, one must consider a variety of factors: Loads, static and dynamic factors, Speed and running pattern, Stiffness, Temperature levels and gradients, heat conduction, Lubrication: viscosity, stiffness, durability, Degree of contamination. Shielding, Mounting, Maintenance, Lifetime and service time. A bearing selection or analysis is futile without rotor dynamic data from the shaft and other rotating parts.

To ensure the long life of a product, many factors have to be taken into account. A poor installation with unfavourable inlet conditions, unfavourable duty points, bad anchoring etc can cause structural disturbances that may be detrimental. While natural frequencies in the structure from poorly designed supports of the pump, pipes, valves etc are often the cause of high vibration levels. These factors describe some of the knowledge and experience including the precautions to be taken into consideration in the design and analysis of shaft and bearings.

II. FAILURE CAUSES

In order to properly dimension the rotating system, the failure causes or modes have to be determined. Most failures are due to unpredictable factors and the cure is to create a robust design that can cope with the unknown. Predictable failures or lifetimes can be calculated although many parameters will vary and statistical considerations have to be taken into account. **2.1 Shaft**

The shaft is designed to have an infinite life. This will be the case unless the shaft is overloaded or damaged.

2.1.1 Fatigue crack

The cause of a broken shaft is almost always fatigue. A crack starts at a stress concentration from a keyway or a sharp radius, or, in rare cases, from a material impurity. Flaws in the surface of a shaft, such as scratches, indents or corrosion, may also be the starting point of a fatigue crack. Loads that drive a crack are normally torsion loads from direct online starts or bending loads from the hydraulic end.

2.1.2 Plastic deformation

Plastic deformation can only occur in extreme load cases when debris is squeezed into a radial clearance that results in large deformations.

2.1.3 Defect in shaft

Defects in shafts that have passed the checks in the factory, checks for unbalance, as well as the check at test run are very rare. On site, however, it is important to prevent damage from corrosion, indents etc, by proper handling.

2.2 Bearing

A bearing does not last forever, sooner or later fatigue or wear, or lubricant deterioration will ultimately destroy the bearings ability to function properly. Bearing failure causes in order of likelihood are listed below.

2.2.1 Penetrating fluid or particles

Particles generate high stresses in the bearing components and thereby create premature fatigue failure. Particles also generate wear that shortens life. Particles, especially light alloy particles like zinc, may act as catalysts for the grease and create premature ageing. Consequently, Nilos rings must not be used! If a fluid enters the bearing and is over rolled the fluid acts as a jet and forces the grease out from the raceway. If the fluid is oil, with just a tiny amount of water (0.1%), the bearing's lifetime is ruined even if it is flooded with that oil. Furthermore, the fluid may also cause corrosion.^[1]

2.2.2 High temperature or gradient

High temperatures due to bad cooling or too much heat generated can be seen (if the bearing is not totally ruined) if the grease has darkened and has a feeling of carbon particles dissolved in oil. If synthetic oil is used, it may have polymerized and created a layer on the surface, mainly seen in oil lubrication. A bearing that has been overfilled with grease may also cause a too high temperature. If the temperature is just slightly higher than allowed, the signs are not so obvious; however, the lifetime will be reduced due to lower viscosity and faster degradation of the lubricant. Cages with plastic material will also age faster at increased temperatures. If too much heat is generated, maybe from overload, but with adequate cooling, then the gradient over the bearing can be too high, generating a preload that can destroy the bearing.^{[2][3]}

III. SHAFT CALCULATIONS

3.1 Torsion Frequency:



3.4 Shaft Deformation:

3.2 Global Reactions:

$$F_{x} = \omega^{2} \cdot Ub_{x}$$

$$z_{x} = \frac{DUb_{xx}}{Ub_{x}}$$

$$F_{x}F_{y} = \text{forces in x and y direction}$$

$$z_{x}z_{y} = \text{position of forces}$$

$$\omega = \text{rotational speed}$$

$$Ub_{x}Ub_{y} = \text{unbalance}$$

$$DUb_{x}DUb_{y} = \text{moment unbalance}$$

3.3 Axial Displacement:

$$\delta = \int_{1}^{\infty} \left[\frac{F \cdot dL}{A \cdot E} + \alpha \cdot dL \cdot \Delta T \right]$$

 $\delta = displacement$

- F = force
- L = length
- E = modulus of elasticity
- A = cross section area
- α = thermal expansion coefficient
- $\Delta T =$ temperature change



cases with equal amplitudes & equal phase^[1]





Figure 3.4.3: The response functions around a single critical frequency for different damping. Max value for 2% damping is 50 and for 5% 20.^[5]



Figure 3.4.4: The deformation of the static run with the sum of the two dynamic runs superimposed at one duty point. Data from start to end of shaft[m].^[6]





Figure 3.8.2: The bending stress of the rotating run with the sum of the static and blade pass runs superimposed in one duty point. *x* and *y* data only. Data from start to end of shaft.^[7]



Figure 3.8.3: The bending stress of the rotating run with *Figure 3.8.4:* The combined and linearized Haigh and Wöhler the sum of the static and blade pass runs superimposed diagram.^[7] diagram.^[7]

IV. STRUCTURAL ANALYSIS IN ANSYS

4.1 Structural Steel Constants :

	TABLE 1			
Structural Steel > Constants				
	Density	7850 kg m^-3		
	Coefficient of Thermal Expansion	1.2e-005 C^-1		
	Specific Heat	434 J kg^-1 C^-1		
	Thermal Conductivity	60.5 W m^-1 C^-1		
	Resistivity	1.7e-007 ohm m		
	Compressive Yield Strength Pa	2.5e+008		
	Tensile Yield Strength Pa	2.5e+008		
	Tensile Ultimate Strength Pa	4.6e+008		
	Strength Coefficient Pa	9.2e+008		
	Cyclic Strength Coefficient Pa	1.e+009		
	Ductility Coefficient	0.213		
	Young's Modulus Pa	2.e+011		
	Poisson's Ratio	0.3		
	Bulk Modulus Pa	1.6667e+011		
	Shear Modulus Pa	7.6923e+010		

TABLE 2				
Model (A4) > Mesh				
Object Name	Mesh			
State	Solved			
Sizing				
Use Advanced Size Function	Off			
Relevance Center	Fine			
Initial Size Seed	Active Assembly			
Smoothing	Medium			
Transition	Fast			
Span Angle Center	Coarse			
Minimum Edge Length	3.2361e-003 m			
Inflation Option	Smooth Transition			

Transition Ratio	0.272			
Maximum Layers	5			
Growth Rate	1.2			
View Advanced Options	No			
Triangle Surface Mesher	Program Controlled			
Statistics				
Nodes	58809			
Elements	33140			

TABLE 3					
Model (A4) > Static Structural (A5) > Loads					
Object Name	Fixed Support	Pressure			
State	Fully Defined				
Scope					
Scoping Method	Geometry Selection				
Definition					
Туре	Fixed Support	Pressure			
Define By		Normal To			
Magnitude		1000. Pa (ramped)			







Figure 4.1.2 : Total Deformation[3D]

Figure 4.1.3 : Maximum Principal Stress[3D]







Figure 4.1.6 : Equivalent Elastic Strain[Section Plane]



Figure 4.1.8 : Equivalent Stress [Section Plane]



Figure 4.1.5 : Equivalent Stress[3D]



Figure 4.1.7 : Total Deformation [Section Plane]



Figure 4.1.9 : Maximum Shear Stress[Section Plane]

IV. CONCLUSION

Looking at the results and all parameters related to the given material which can be used for the bearing one can conclude that the bearing is safe under given load conditions as the values of Equivalent Elastic Strain, Total Deformation, Equivalent Stress and Maximum Shear Stress are seen towards the respective parameters related to the material which we have considered.

Area which is under high stresses is easily recognized and the future scope could be the working on that area by considering the various factors like CFD analysis and thermal analysis.

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REFERENCES

[1]ITT Flygt 892933 CT-design. Design recommendations for pumping stations with dry installed submersible pumps.
[2]Gert Hallgren Thermal Analysis of Electrical Pump Motors. The ITT Flygt Scientific Impeller No. 5, p56-62 (1998)
[3]Per Strinning A computerized trial and error technique for impeller design. The ITT Flygt Scientific Impeller No. 3, p19-27.
[4]Thomas Börjesson Time accurate simulation of a centrifugal pump. The ITT Flygt Scientific Impeller No. 6, p21-30 (1998)
[5]Ioannides E., Harris T.A. A new fatigue life model for rolling contacts. Trans ASME JoT, Vol 107 p367-378 (1985)
[6]Ioannides E., Bergling G, Gabelli A. The SKF formula for rolling bearing. SKF magazine Evolution no 1, p25-28 (2001)
[7] Johannes Brändlein, Paul Eschmann, Ludwig Hasbargen, Karl Wiegand. Ball and roller bearings, design and application.

